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COUPLING CONDITIONS FOR THE TRANSITION FROM SUPERSONIC TO SUBSONIC FLUID STATES

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ABSTRACT. We discuss coupling conditions for the p-system in case of a transition from supersonic states to subsonic states. A single junction with adjacent pipes is considered where on each pipe the gas flow is governed by a general p-system. By extending the notion of demand and supply known from traffic flow analysis we obtain a constructive existence result of solutions compatible with the introduced conditions.

1. Introduction. Natural gas pipeline transportation systems are an important part of our infrastructure. Besides transport of gas, also CO_2 pipeline transport plays an important role in carbon capture and storage, see for example [18]. A well–established mathematical model for such flow is the p–system (1). The p–system in conservative variables density $\rho > 0$ and flux q is given by

$$\partial_t \rho(t,x) + \partial_x q(t,x) = 0, \ \partial_t q(t,x) + \partial_x \left(\frac{q^2(t,x)}{\rho(t,x)} + p(\rho(t,x))\right) = 0, \tag{1}$$

where $t \ge 0$ is time, x is space, and $\rho \to p(\rho)$ is the pressure law. The system is stated in Eulerian coordinates and it is a simplified model for gas flow in pipes [21] or water flow in open canals [11]. In the latter case $\rho = h$ is the water height and $p(h) = \frac{g}{2}h^2$ with g denoting the gravitational acceleration. We are interested in the situation of a single junction connected to pipes depicted in Figure 1. The pipes are modeled as directed arcs and the junction as node. We suppose to have n incoming pipes parameterized by $x \in (-\infty, 0]$ and labeled by $k \in \delta^- := \{-n, \ldots, -1\}$. Similarly, we suppose to have m outgoing pipes $k \in \delta^+ := \{1, \ldots, m\}$ and parameterized by $x \in [0, \infty)$. Along each pipe the evolution of the gas is supposed to fulfill (1) and the state of the system in pipe k is denoted by $U_k := (\rho_k, q_k)^t$. The dynamics of the pipes is then coupled at x = 0 through coupling conditions [2]. General results on

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the p-system at a junction are given in [9]. For a recent overview of theoretical and numerical results for flows on networks governed by hyperbolic equations we refer to [4]. Except for [14] all current coupling conditions rely on a transversality condition [10] to establish well-posedness. This condition is replaced here by a solvability condition prior to Theorem 2.3 having a similar meaning, namely, that Lax curves are not parallel in the point of intersection in phase space.



FIGURE 1. Junction of $n + m = |\delta^-| + |\delta^+|$ connected pipes.

It has been shown that the transversality condition is fulfilled for subsonic data, i.e. initial conditions $U_i^0(x)$ with $i \in \delta^+ \cup \delta^-$ fulfilling $\lambda_1(U_i^0) < 0 < \lambda_2(U_i^0)$ where $\lambda_j, j = 1, 2$ are the characteristic velocities given by equation (5). To the best of our knowledge, no results in the supersonic case exist. However, in the scalar case on networks this case has been well-understood and discussed intensively, see for example [17, 6] or [12]. We are interested in the coupling of *supersonic* and *subsonic* states for the p-system. We focus on the most common coupling condition for gas networks as well as coupled open canals, namely, we prescribe

$$p(\rho_k(t, 0+)) = p^*(t) \ \forall k \in \delta^+, \ p(\rho_k(t, 0-)) = p^*(t) \ \forall k \in \delta^-,$$
(2a)

$$\sum_{k \in \delta^{-}} q_k(t, 0-) = \sum_{k \in \delta^{+}} q_k(t, 0+).$$
(2b)

for some unknown nodal pressure $p^*(t)$ and where $0\pm$ denote the trace values coming from the interior of the pipe. We refer to [2, 15, 9] for a more detailed discussion of coupling conditions. Our main result is Theorem 2.3 showing that there exists a solution to the coupling conditions (2) under suitable assumptions on the initial data. The key assumption is on the sign eigenvalues of the initial datum, i.e., equation (17). Briefly summarized the assumption states that the data on incoming arcs is supersonic and the data on outgoing arcs is subsonic.

The study of the coupling of subsonic and supersonic flow is also important for algorithmic purposes. For example in an iterative method for the solution of optimal control problems (see for example [7]), it can happen that during the iteration in an intermediate step, supersonic states appear even if the optimal state is subsonic. The transition from supersonic to subsonic flow is important for high-speed aircraft, where a supersonic external freestream flow must be decelerated efficiently to subsonic speed at the turbine inlet. This transition from supercritical flow to subcritical flow also occurs in Fanno flows, see [22], (p. 199). The transition from supercritical to subcritical regime in free surface flow of yield stress fluids has been

studied in [23] where a hydraulic jump during laminar flow of an Herschel-Bukley fluid in a rectangular channel is studied. An experimental assessment of scale effects affecting two-phase flow properties in hydraulic jumps is given in [20].

In this work we will introduce a notion of supply and demand for the state of the system on the adjacent pipes similar to the notion in traffic flow [19, 14]. This will allow to solve for constant initial data $U_k^0 = cst$ the problem (1) and (2) also in the supersonic case. Necessary conditions on the constants U_k^0 are presented ensuring solvability. In the case of n = m = 1 the solution coincides with a classical solution to a Riemann problem.

2. Theoretical results. We recall the Lax–curves for the p–system for a pressure law satisfying the following assumption on the equation of state, i.e. $p \in C^3(\mathbb{R}^+; \mathbb{R}^+)$ with

$$p'(\rho) > 0, \ p''(\rho) \ge 0,$$
 (3a)

$$6p'(\rho) + 3p''(\rho)(\rho - \overline{\rho}) + \rho \left(3p''(\rho) + (\rho - \overline{\rho})p'''(\rho)\right) > 0 \quad \forall \rho > \overline{\rho} \ge 0 \tag{3b}$$

and such that $p(\rho), p'(\rho) \to 0$ for $\rho \to 0$. Note that the first condition (3a) implies the usual assumption on the equation of state

$$\rho p''(\rho) + 2p'(\rho) > 0, \tag{4}$$

see e.g. [9, 5]. This also implies that both characteristic fields are genuinely nonlinear. In addition, the second condition (3b) is required later in order to obtain strict convex (resp. concave) wave curves. The assumptions (3) are fulfilled by the pressure law of the isentropic Euler equations $p(\rho) = \rho^{\gamma}$ for $\gamma > 1$ as well as for the shallow-water equations where the hydrostatic pressure is $p(\rho) = \frac{g}{2}\rho^2$. In particular, the isothermal equation $p(\rho) = \rho$ is frequently applied in network simulations. We note that a sufficient condition for (3b) is $p'''(\rho) \ge 0$ that for isentropic Euler equations only holds for $\gamma \ge 2$.

Under the assumption (3a) the p-system (1) is strictly hyperbolic in the non-vacuum states $\{U : \rho > 0\}$. The speed of sound is given by $c(\rho) = \sqrt{p'(\rho)}$ and the eigenvalues of the *i*th characteristic field are for i = 1, 2

$$\lambda_1(U) = \frac{q}{\rho} - c(\rho), \ \lambda_2(U) = \frac{q}{\rho} + c(\rho).$$
 (5)

Both characteristic fields are genuinely nonlinear if the equation of state fulfills (4) and (3a). The 1–Lax–curve through $\overline{U} = U_{\ell}$ is given by

$$L_1(\sigma; \overline{U}) = \begin{pmatrix} R_1(\sigma; \overline{U}) & \sigma \le \overline{\rho} \\ S_1(\sigma; \overline{U}) & \sigma > \overline{\rho} \end{pmatrix}.$$
 (6)

The reversed 2–Lax–curve through $\overline{U} = U_r$ is given by

$$L_2^-(\sigma;\overline{U}) = \begin{pmatrix} S_2(\sigma;\overline{U}) & \sigma > \overline{\rho} \\ R_2(\sigma;\overline{U}) & \sigma \le \overline{\rho} \end{pmatrix}.$$
 (7)

Here, for i = 1, 2 we have the positive and negative branch of

$$S_{i}(\sigma;\overline{U}) = \sigma \ \frac{\overline{q}}{\overline{\rho}} \mp \sqrt{\frac{\sigma}{\overline{\rho}}} (\sigma - \overline{\rho})(p(\sigma) - p(\overline{\rho})),$$
$$R_{i}(\sigma;\overline{U}) = \sigma \frac{\overline{q}}{\overline{\rho}} \mp \sigma \int_{\overline{\rho}}^{\sigma} \frac{c(s)}{s} ds.$$

The precise form and derivation of the curves can be found e.g. in [9, 13]. Therein, also the following properties are established: The shock curves S_i , i = 1, 2, are

concave and convex with respect to U in the ρ -q-plane. The rarefaction curves R_i , i = 1, 2, are concave and convex, respectively, in the ρ -q-plane. The Riemann problem has a global unique solution, see [5, Section 6.3]. The remaining Lax curves are given for example in [9, Equation 4.1, Equation 4.2].

From the explicit form of R_i we obtain

$$\frac{d^2}{d\sigma^2}R_i(\sigma,\overline{U}) = \mp \left(\frac{\sigma p^{\prime\prime}(\sigma) + 2p^\prime(\sigma)}{2\sigma\sqrt{p^\prime(\sigma)}}\right)$$

Since $\sigma > \overline{\rho} > 0$, the discriminant $s(\sigma) = \frac{\sigma}{\overline{\rho}}(\sigma - \overline{\rho})(p(\sigma) - p(\overline{\rho}))$ in $S_i(\sigma; \overline{U})$ is positive. Furthermore, due to assumption (3), s is strict convex, i.e.

$$s''(\sigma) = 2\frac{\sigma}{\overline{\rho}}p'(\sigma) + \frac{2}{\overline{\rho}}(p(\sigma) - p(\overline{\rho})) + \frac{\sigma - \overline{\rho}}{\overline{\rho}}\left(2p'(\sigma) + \sigma p''(\sigma)\right) > 0.$$

Hence,

$$\frac{d^2}{d\sigma^2}S_i(\sigma,\overline{U}) = \mp \frac{1}{2\sqrt{s(\sigma)}} \left(s''(\sigma) - \frac{s'(\sigma)^2}{2s(\sigma)}\right).$$

The function $\tilde{s}(\sigma) = 2s''(\sigma)s(\sigma) - s'(\sigma)^2$ vanishes at $\sigma = \overline{\rho}$ and $\tilde{s}'(\sigma) = 2s'''(\sigma)s(\sigma)$. We also note that

$$s^{\prime\prime\prime}(\sigma)\overline{\rho} = 6p^{\prime}(\sigma) + 3p^{\prime\prime}(\sigma)(\sigma - \overline{\rho}) + \sigma\left(3p^{\prime\prime}(\sigma) + (\sigma - \overline{\rho})p^{\prime\prime\prime}(\sigma)\right) > 0$$

provided that condition (3b) holds true. Then, \tilde{s} is a monotone increasing function for all $\sigma > \bar{\rho}$ starting at zero. This yields the strict concavity and convexity of S_i , respectively.

Under assumption (3b) we therefore obtain

$$S_i$$
 is strictly concave and R_i is strictly convex, $i = 1, 2.$ (8)

Hence, L_1 and L_2^- have a single maximum and minimum, respectively. We denote by $q^* = q^*(\overline{U})$ the maximum of the functions $\rho \to L_1(\rho; \overline{U})$ and $\rho \to -L_2^-(\rho; \overline{U})$. The corresponding density is denoted by $\rho^* = \rho^*(\overline{U})$. The Heaviside function is denoted by H(x).

2.1. The notion of demand and supply for the p-system. We now define the demand and supply for the p-system extending the notion in the scalar case [19]. In the ρ -q-plane and for $\rho > 0$ the demand $\rho \mapsto d(\rho; \overline{U})$ is an extension of the non-decreasing part of the curve $\rho \mapsto L_1(\rho; U)$. In the ρ -q-plane and for $\rho > 0$ the supply function $\rho \mapsto s(\rho; \overline{U})$ is an extension of the non-increasing part of the curve $\rho \mapsto -L_2^-(\rho; U)$. The maximum of L_1 and $-L_2^-$ depend on \overline{U} . For readability we skip this dependence in the following formulas for d and s.

$$d(\rho;\overline{U}) = \begin{pmatrix} L_1(\rho;\overline{U}), & 0 < \rho \le \min\{\overline{\rho}, \rho^*\} \\ \overline{q} \ H(\rho^* - \overline{\rho}) + q^* \ H(\overline{\rho} - \rho^*), & \text{else} \end{pmatrix}$$
(9)

$$s(\rho;\overline{U}) = \begin{pmatrix} L_2^-(\rho;\overline{U})H(\rho-\rho^*) - q^*H(\rho^*-\rho), & \overline{\rho} > \rho^* \\ \overline{q}H(\overline{\rho}-\rho) + H(\rho-\overline{\rho})\max\{\overline{q}, L_2^-(\rho;\overline{U})\}, & \overline{\rho} < \rho^* \end{pmatrix}.$$
 (10)

A sketch of the supply and demand for different states $\overline{U} = (\overline{\rho}, \overline{q})$ is given in Figure 2 and Figure 3, respectively.

The demand and supply are used to determine admissible fluxes for waves of non–positive and non–negative speed, respectively. A Riemann problem is a Cauchy problem for equation (1) and initial data $U_0(x) = \begin{pmatrix} U_\ell & x < 0 \\ U_r & x > 0 \end{pmatrix}$. A weak solution



FIGURE 2. The supply function $\rho \mapsto s(\rho; \overline{U})$ in red for given data \overline{U} indicated by a cross for $\overline{\rho} > \rho^*$ (left) and $\overline{\rho} < \rho^*$ (right). Also shown in blue is the curve L_2^- . The state U^* is indicated by a circle.



FIGURE 3. The demand function $\rho \mapsto d(\rho; \overline{U})$ in red for given data \overline{U} . Also shown in blue is the curve L_1 .

to the Riemann problem is defined e.g. in [3] and consists of a superposition of self– similar waves. In the case of the 2×2 system we obtain at most two waves separated by an intermediate state. The general structure in the present case therefore is a superposition of either a shock or rarefaction wave of the first family with a shock or rarefaction wave of the second family.

Theorem 2.1. Let \overline{U} with $\overline{\rho} > 0$ be given and assume (3). Then, for all $q \leq d(\overline{\rho}; \overline{U})$, there exists a state $\tilde{U} = (\tilde{\rho}, q)$ such that the Riemann problem for (1) with $U_{\ell} = \overline{U}$ and $U_r = \tilde{U}$ admits a weak self-similar solution composed of waves of non-positive speed.

Proof. We have to distinguish two cases. Suppose $\overline{\rho} < \rho^*(\overline{U})$, see Figure 3 (right). Then, $d(\overline{\rho}; \overline{U}) = \overline{q}$. Denote by $\tau \neq \overline{\rho}$ the value of ρ , such that $\overline{q} = L_1(\tau; \overline{U})$. Due to the strict concavity of L_1 and for $q < d(\overline{\rho}; \overline{U})$ there exists a unique density $\tilde{\rho} > \tau$, such that $L_1(\tilde{\rho}; \overline{U}) = q$. The solution to the Riemann problem consists of a single shock propagating with non-positive velocity. Suppose $\overline{\rho} < \rho^*(\overline{U})$ and assume $q = \overline{q} = d(\overline{\rho}; \overline{U})$. Then, $\tilde{U} = \overline{U}$ as well as $\tilde{U} = (\tau, q)$ where $\tau \neq \overline{\rho}$ fulfills $L_1(\tau; \overline{U}) = q$. Note that in the latter case the solution is a shock of zero speed. Since this is a stationary discontinuity located at a single point we can exclude this solution from our construction as in [16]. In the case $\overline{\rho} > \rho^*(\overline{U})$, see Figure 3 (left), we obtain $d(\overline{\rho}; \overline{U}) = q^*(\overline{U})$. For $\overline{q} \leq q \leq q^*(\overline{U})$ we find a density $\tilde{\rho}$ such that $\rho^* \leq \tilde{\rho}(\overline{U}) \leq \overline{\rho}$ and $q = L_1(\tilde{\rho}; \overline{U})$. The solution to the corresponding Riemann problem consists of a rarefaction wave with non–positive speed. For $q < \overline{q}$, we find $\tilde{\rho} > \overline{\rho}$ and $q = L_1(\tilde{\rho}; \overline{U})$, such that the solution to the corresponding Riemann problem consists of a shock of negative speed.

Corollary 1. Let \overline{U} with $\overline{\rho} > 0$ be given and assume (3). Then, for all $q \ge s(\overline{\rho}; \overline{U})$, there exists a state $\tilde{U} = (\tilde{\rho}, q)$ such that the Riemann problem for (1) with $U_{\ell} = \tilde{U}$ and $U_r = \overline{U}$ admits a weak self-similar solution composed of waves of non-negative speed.

The proof is similar to the proof of Theorem 2.1 and omitted. It should be noted that in the formulation of Corollary 1 the right state \overline{U} is given instead of the left state in Theorem 2.1.

2.2. The coupling at a single junction. We introduce the following subsets of $\mathbb{R}^+ \times \mathbb{R}$ depending on the sign of the eigenvalues λ_i given by (5).

$$A^{+} := \{ U := (\rho, q) : \lambda_{i}(U) > 0, \ i = 1, 2 \},$$
(11)

$$A := \{ U := (\rho, q) : \lambda_1(U) < 0 < \lambda_2(U) \},$$
(12)

$$A^{-} := \{ U := (\rho, q) : \lambda_i(U) < 0, \ i = 1, 2 \}.$$

The set A comprises of the states in the subsonic region, $A^+ \cup A^-$ is the supersonic region. For the junction located at x = 0 we consider the Riemann problem

$$\partial_t \begin{pmatrix} \rho_k(t,x) \\ q_k(t,x) \end{pmatrix} + \partial_x \begin{pmatrix} q_k(t,x) \\ \frac{q_k^2(t,x)}{\rho_k(t,x)} + p(\rho_k(t,x)) \end{pmatrix} = 0, \ U_k(t,0) = \begin{pmatrix} U_k^- & x < 0 \\ U_k^+ & x > 0 \end{pmatrix}.$$
(13)

Depending on the pipe only one of the Riemann data is defined at t = 0, i.e. $U_k^- = U_{0,k}$ if $k \in \delta^-$ and $U_k^+ = U_{0,k}$ if $k \in \delta^+$. For each pipe the remaining unknown state U_k^{\pm} for $k \in \delta^{\pm}$ is determined in such a way that equation (2) holds true. We construct a Riemann solver at the node $(U_k(t, x))_{k \in \delta^{\pm}}$ to (13) and (2). An explicit construction is provided for constant initial data self-similar solutions $U_k(t, x)$ consisting of wave of non-positive speed and non-negative speed for $k \in \delta^-$ and $k \in \delta^+$, respectively. This solution is restricted to $U_k(t, x)$ for x < 0 and x > 0, when $k \in \delta^-$ and $k \in \delta^+$, respectively.

The demand and supply allows to construct solutions of certain wave speeds. Consider $k \in \delta^-$. Let $U_k^- := U_{0,k}$ and $q \leq d(\rho_{0,k}; U_{0,k})$ be given. Then, according to Theorem 2.1, there exist a state U_k^+ with $q_k^+ = q$ and such that the Riemann problem (13) admits a solution $U_k(t, x)$. The solution consists of a wave of non-positive speed. Similarly, for $k \in \delta^+$, data $U_k^+ := U_{0,k}$ and any $q \geq s(\rho_{0,k}; U_{0,k})$ a self-similar solution $U_k(t, x)$ consisting of waves of non-negative speed exist according to Corollary 1.

In order to obtain a unique density at the node we define the function $\overline{U} \mapsto \tau_k(\overline{U})$ by

$$k \in \delta^{-} : \tau_{k}(\overline{U}) := \begin{pmatrix} \rho^{*}(\overline{U}) & \text{if } \overline{\rho} \ge \rho^{*}(\overline{U}), \\ \widetilde{\rho} & \text{else} \end{pmatrix}, \text{ where } \widetilde{\rho} \neq \overline{\rho} \text{ and } L_{1}(\widetilde{\rho}; \overline{U}) = \overline{q}.$$
(14a)

Similarly,

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$$k \in \delta^{+}: \tau_{k}(\overline{U}) = \begin{pmatrix} \rho^{*}(\overline{U}) & \text{if } \overline{\rho} \ge \rho^{*}(\overline{U}), \\ \widetilde{\rho} & \text{else} \end{pmatrix}, \text{ where } \widetilde{\rho} \neq \overline{\rho} \text{ and } L_{2}^{-}(\widetilde{\rho}; \overline{U}) = \overline{q}.$$
(14b)

Clearly, $\tau_k > 0$ if $\overline{\rho} > 0$. τ_k is well-defined due to equation (8). For $k \in \delta^-$ and $\overline{\rho} < \rho^*(\overline{U})$ we obtain $L_1(\tau_k(\overline{U}); \overline{U}) = L_1(\overline{\rho}; \overline{U}) = \overline{q}$. Hence, in this case $\tau_k(\overline{U})$ is the density such that the wave connecting $U_\ell = (\overline{\rho}, \overline{q})$ and $U_r = (\tau_k(\overline{U}), \overline{q})$ has zero speed and is omitted as in the proof of Theorem 2.1.

Finally, we turn to the description of the Riemann solver for problem (13) and (2). Due to assumption (3) we have that the condition (2) is equivalent to

$$\rho_k(t, 0+) = \rho_{k'}(t, 0-) \ \forall k \in \delta^+, k' \in \delta^-,$$
(15)

and

$$\sum_{k\in\delta^{-}} q_k(t,0-) - \sum_{k\in\delta^{+}} q_k(t,0+) = 0.$$
(16)

Note that in the case n = m = 1, i.e. $\delta^{\pm} = \{\pm 1\}$, the conditions (15) and (2) imply by means of the Rankine-Hugoniot jump conditions in particular

$$q_{-1}(t,0-) = q_1(t,0+), \ \frac{q_{-1}^2(t,0-)}{\rho_{-1}(t,0-)} + p(\rho_{-1}(t,0-)) = \frac{q_1^2(t,0+)}{\rho_1(t,0+)} + p(\rho_1(t,0+)).$$

For consistency a solution to (13) should therefore be also a solution to a (classical) Riemann problem for (1) with initial data $U(0, x) = \begin{pmatrix} U_{-1}^- & x < 0 \\ U_1^+ & x > 0 \end{pmatrix}$.

We are interested in supersonic and subsonic coupling at the junction. Therefore, we assume in the following that

$$U_k^- = U_{0,k} \in A^+ \text{ for } k \in \delta^-, \ U_k^+ = U_{0,k} \in A \text{ for } k \in \delta^+.$$
 (17)

Remark 1. Due to the symmetry of the Lax curves for the p–system, the discussion also includes the case where $U_k^- \in A$ for $k \in \delta^-$ and $U_k^+ \in A^-$ for $k \in \delta^+$. The case $U_k^{\pm} \in A$ for $k \in \delta^{\pm}$ has been discussed for example in [8].

We now plan to construct a solution fulfilling the coupling conditions. As preliminary result we prove the monotonicity of the Lax curves.

Lemma 2.2. Assume $U_{0,k}$ for $k \in \delta^{\pm}$ with $\rho_{0,k} > 0$ are given. Suppose further that (3) holds true.

Then, for all $\sigma \geq \sigma_{lb}$ we have that $\sigma \mapsto L_1(\sigma; U_{0,k})$ for $k \in \delta^-$ is strictly monotone decreasing and $\sigma \mapsto L_2^-(\sigma; U_{0,k})$ for $k \in \delta^+$ is strictly monotone increasing.

Proof. In the case $\rho_{0,k} < \rho^*(U_{0,k})$ we have that $\tau_k(U_{0,k}) > \rho^*(U_{0,k})$ by definition (14). Therefore, the proof follows from the monotonicity properties of $L_1(\cdot)$ and $L_2^-(\cdot)$, respectively. The monotonicity implies that $\sigma \mapsto \sum_{k \in \delta^-} L_1(\sigma; U_{0,k})$ and $\sigma \mapsto \sum_{k \in \delta^+} L_2^-(\sigma; U_{0,k})$ are monotone decreasing and increasing in $[\sigma_{lb}, \infty)$, respectively. Furthermore, $L_1(\sigma_{lb}; U_{0,k}) \leq d(\sigma_{lb}; U_{0,k}), k \in \delta^-$ and $L_2(\sigma_{lb}; U_{0,k}) \geq s(\sigma_{lb}; U_{0,k}), k \in \delta^+$. This finishes the proof.

In general, under assumption (17), the solution to a Riemann problem for (1) consists of a superposition of waves of the first family and waves of the second family. In order to solve the problem (13) we mimic this behavior by constructing of a solution as follows. Denote by

$$\tau_{lb} := \max_{k \in \delta^{\pm}} \tau_k(U_{0,k}). \tag{18}$$

Then, equation (16) is fulfilled provided that there exists σ with $\sigma \geq \sigma_{lb}$ and (16)

$$\sum_{k \in \delta^{-}} L_1(\sigma; U_{0,k}) - \sum_{k \in \delta^{+}} L_2^{-}(\sigma; U_{0,k}) = 0.$$
(19)

The following Theorem guarantees the solvability of the previous equation and presents the main result.

Theorem 2.3. Assume $U_{0,k}$ for $k \in \delta^{\pm}$ with $\rho_{0,k} > 0$ are given. Suppose further that (3) holds true. Let σ_{lb} be given by equation (18). Provided that

$$\sum_{k \in \delta^{-}} L_1(\sigma_{lb}; U_{0,k}) \ge \sum_{k \in \delta^{+}} L_2^-(\sigma_{lb}; U_{0,k})$$
(20)

there exists a unique $\sigma \geq \sigma_{lb}$, such that equation (19) is fulfilled.

The proof follows immediately from the monotonicity properties established before.

Now, we continue our construction: Suppose (19) has a unique solution $\overline{\sigma}$, see Theorem 2.3. Then, define

$$U_k^+ := \left(\overline{\sigma}, L_1(\overline{\sigma}; U_{0,k})\right)^T, k \in \delta^-, \ U_k^- := \left(\overline{\sigma}, L_2^-(\overline{\sigma}; U_{0,k})\right)^T, k \in \delta^+.$$
(21)

Then, we have $L_1(\overline{\sigma}; U_{0,k}) \leq d(\rho_{0,k}; U_{0,k})$ for $k \in \delta^-$ and $L_2^-(\overline{\sigma}; U_{0,k}) \geq s(\rho_{0,k}; U_{0,k})$ for $k \in \delta^+$ due to Lemma 2.2. According to Theorem 2.1 and Corollary 1 this ensures that the solution to problem (13) has non–positive and non–negative speed, respectively. Therefore, a solution to the problem (13) fulfills equation (16) and (15).

Some remarks are in order.

Remark 2. Note that this construction is also valid in the case $U_k^- \in A$ and coincides with the solution to the equal pressure condition proposed in [8, 2].

In the case n = m = 1 we have $U_{-1}^+ = U_1^- =: \overline{U}$. Since $\lambda_1(\overline{U}) < \lambda_2(\overline{U})$ the solution (13) consists by construction of at most a wave of the first family on k = -1. On k = 1 we may have at most a wave of the second family. This is consistent with the solution to a Riemann problem (13) with initial data $U(0, x) = \begin{pmatrix} U_{-1}^- & x < 0 \\ U_1^+ & x > 0 \end{pmatrix}$.

Remark 3. Note that linearization techniques in order to solve (2) and (16) will fail to provide a solution to (13) due to the fact that at $U_{0,k}, k \in \delta^-$ both eigenvalues are non-negative. Therefore, a linear system obtained through linearization at $U_{0,k}, k \in \delta^{\pm}$ would have only *m* degrees of freedom to prescribe boundary conditions. However, the given set of conditions are in fact n + m. This is different compared with the case $U_{0,k} \in A$ for all $k \in \delta^{\pm}$.

In the case $U_{0,k} \in A^-$ for $k \in \delta^+$ the problem (13),(15) and (16) is more complicated in the following way. The characteristic families can no longer be uniquely related to whether they are incoming $(k \in \delta^-)$ or outgoing $(k \in \delta^+)$. One can easily find examples such that we observe two waves of different families on the outgoing and a wave on the incoming pipe. Therefore, new additional conditions have to be imposed to treat the additional degree of freedom.

2.3. **Example.** We consider $p(\rho) = \rho^2$ as an example. Further, we assume $\delta^- = \{-3, \ldots, -1\}$ and $\delta^+ = \{1, \ldots, 4\}$. Initial data $U_{0,k}$ is chosen randomly such that $U_{0,k} \in A^+$ for $k \in \delta^-$ and $U_{0,k} \in A$ for $k \in \delta^+$. The initial data $U_{0,k}$ does not fulfill the coupling condition (16) and (15) as seen in Table 1. We then compute

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the states at the junction (21) according to the discussion of the previous section. Numerically, we solve equation (19) using Newton's method. The results are given in Table 2. As expected the density and the pressure fulfill (2) and (15). Further, we report on the difference between incoming and outgoing fluxes. The equation (19) has been solved up to machine precision.

Pipe k	$(\rho_{0,k}, q_{0,k})$	$p(\rho_{0,k})$
-1	(5.151e-01, 2.519e+00)	2.653e-01
-2	(6.317e-01, 2.794e+00)	3.991e-01
-3	(6.642e-01, 3.905e+00)	4.412e-01
1	(5.730e-01, -2.648e-01)	3.283e-01
2	(7.460e-01, -1.523e-01)	5.565e-01
3	(5.931e-01, -1.280e-01)	3.518e-01
4	(5.849e-01, 6.020e-01)	3.421e-01

TABLE 1. Random initial states $U_{0,k}$ on incoming pipes k < 0 and outgoing pipes k > 0. The initial difference in the sum of the mass fluxes is given by $\Delta = 9.162e + 00$.

Pipe k	(ho_k, q_k)	$p(\rho_k)$
-1	(2.089e+00, 5.101e+00)	4.364e + 00
-2	(2.089e+00, 4.868e+00)	4.364e + 00
-3	(2.089e+00, 8.090e+00)	4.364e + 00
1	(2.089e+00, 3.757e+00)	4.364e + 00
2	(2.089e+00, 3.357e+00)	4.364e + 00
3	(2.089e+00, 4.147e+00)	4.364e + 00
4	(2.089e+00, 6.798e+00)	4.364e + 00

TABLE 2. Terminal states $U_k(t, 0\pm)$ for $k \in \delta^{\pm}$. The difference in the sum of the mass fluxes is zero.

3. Summary. While coupling conditions for the subsonic flow in gas pipelines are well-established, in this paper the coupling conditions for the transonic transition from supersonic flow to subsonic flow are studied that have not been thoroughly analyzed before. In this way we fill a gap in the theory, which is important in order to have a complete theory that covers all cases. This can also be important for algorithmic purposes, since during an iterative method for the solution of an optimal control problem, it may happen that supersonic states occur, even if the optimal state is subsonic. The purely subsonic case has been treated explicitly in [1] and in general e.g. in [8]. For a complete theory of all possible cases the fully supersonic case is still at large. Future work may then include a complete statement provided the challenges in the supersonic regime can be dealt with.

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