

*Research article***A virtual power plant model for time-driven power flow calculations****Gerardo Guerra and Juan A. Martinez Velasco ***

Departament d'Enginyeria Electrica, Universitat Politecnica de Catalunya, Av. Diagonal 647, 08028 Barcelona, Spain

*** Correspondence:** Email: martinez@ee.upc.edu; Tel: +3-493-401-6725.

Abstract: This paper presents the implementation of a custom-made virtual power plant model in OpenDSS. The goal is to develop a model adequate for time-driven power flow calculations in distribution systems. The virtual power plant is modeled as the aggregation of renewable generation and energy storage connected to the distribution system through an inverter. The implemented operation mode allows the virtual power plant to act as a single dispatchable generation unit. The case studies presented in the paper demonstrate that the model behaves according to the specified control algorithm and show how it can be incorporated into the solution scheme of a general parallel genetic algorithm in order to obtain the optimal day-ahead dispatch. Simulation results exhibit a clear benefit from the deployment of a virtual power plant when compared to distributed generation based only on renewable intermittent generation.

Keywords: distribution system; energy resource; energy storage system; OpenDSS; photovoltaic generation; power flow; virtual power plant; wind generation

1. Introduction

The increasing penetration of renewable generation has been motivated by the necessity of reducing the current dependence on non-renewable energy sources. Solar and wind power systems are two of the most widespread forms of electricity generation based on renewable energy resources. The modular nature of these technologies makes them a suitable option for the deployment of small scale generation connected at distribution level, namely as distributed generation (DG).

DG can be used for supporting voltage, reducing losses, providing backup power and ancillary services, or deferring distribution system upgrade [1,2,3]. However, the intermittent nature of some

renewable resources (e.g. solar and wind) complicates their integration into the grid as they cannot be properly dispatched. In general, renewable generation is permitted to produce as much power as the resource availability allows; this approach limits the integration of renewable DG since unacceptable operating conditions may appear under large penetration scenarios (e.g. system voltages above accepted limits).

Energy storage (ES) capabilities can be used to improve network operation and compensate the intermittency of renewable generation [4–7]. Through the aggregation of renewable DG and ES, it is possible to constitute an entity, known as a virtual power plant (VPP), which can operate as a single dispatchable power plant [8,9]. As part of a VPP, ES can be charged when there is a generation excess and provide support to meet the dispatched power when DG generation decreases.

This paper presents the implementation of a custom-made VPP model for power flow calculations in OpenDSS [10]. The objective is to present a model based on the storage object available in OpenDSS, adequate for distribution system studies and quasi-static (time-driven) simulations. The VPP model has been compiled within the OpenDSS COM DLL and can be used in simulations driven from other software platforms, e.g. MATLAB.

The paper is organized as follows. Section 2 details the configuration and operation of the implemented model. A case study aimed at demonstrating the model behavior is presented in Section 3. The optimization of the hourly day-ahead dispatch using a genetic algorithm (GA) is explored in Section 4. The main conclusions drawn from the paper, as well as future work, are summarized in Section 5.

2. VPP Model for Power Flow Calculations

2.1. VPP definition

A VPP can be defined as a flexible representation of a portfolio of distributed energy resources (DERs), in which a single operating profile can be created from a composite of parameters characterizing each DER [11]. Through the aggregation of DERs it is possible for the VPP to operate as a system-connected power plant and have access to wholesale energy markets and provide support services for the transmission system management.

VPPs can be classified as commercial VPP (CVPP) or technical VPP (TVPP) [11]. A number of DERs can participate in the energy market as a single CVPP, while the TVPP models the characteristics of a system that contains an aggregation of DERs, and acts as a single power plant. The CVPP can represent resources from different locations, whereas all DERs in a TVPP belong to the same geographical location.

The main elements that compose a VPP are: (i) energy production units, (ii) energy storage units, and (iii) flexible loads [12]. The VPP must exert control over the different elements in order to coordinate and optimize their operation. VPP control is conducted via a communication system that connects all the DERs in the VPP [8,13].

A VPP can also be defined as an aggregation of power production from a group of grid-connected DERs operated by a centralized controller [9]. According to this definition, the combination of DG and ES with a coordinated control can also be considered as a VPP, since it allows them to operate as a single dispatchable power plant. Although exporting energy to the transmission system is still possible (by reversing the power flow through the substation transformer),

the VPP's main task will be to provide support to the distribution network as dispatchable DG. The model presented in this section corresponds to this definition of VPP and only considers the aggregation of energy storage and renewable generation, either photovoltaic (PV) or wind.

2.2. VPP configuration and components

The general configuration of the VPP model is shown in Figure 1; it is composed by a generation unit (GU), an ES unit, and an inverter. In this configuration the GU, which can be either solar or wind generation, and the ES are connected at DC level. The VPP will be referred to as Solar VPP or Wind VPP depending on the nature of the renewable resource used in the GU. The VPP is capable of injecting or absorbing reactive power through the inverter. The required parameters for each component are listed in Table 1.

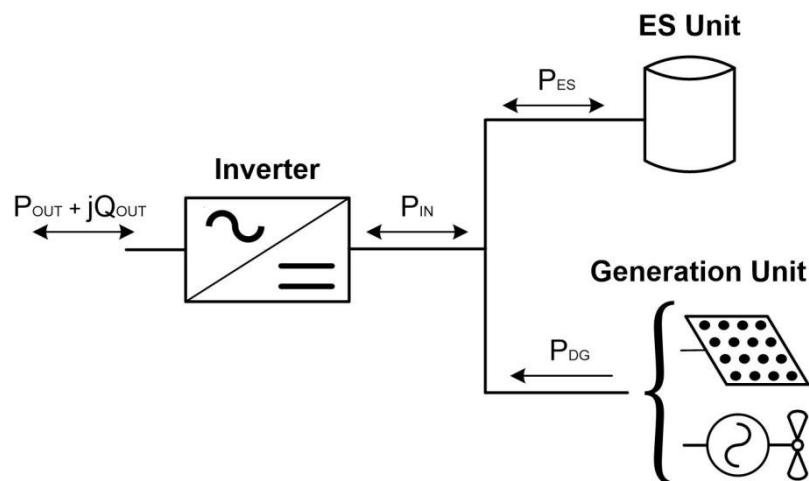


Figure 1. Basic configuration of the virtual power plant.

PV Generator: The power produced by a PV generator is a function of the irradiance, panel temperature, and rated power at a selected temperature and an irradiance of 1.0 kW/m^2 [10]. It is assumed that the model can operate at maximum power or reduce the generated power according to the power curtailment parameter. Furthermore, the PV generator will only inject power if the generated power is above the predetermined minimum power, which is defined as a percentage of the rated power.

Wind Generator: The output power produced by the wind generator is calculated following the procedure presented in [14]. The wind generator is defined by its rated power, hub height, cut-in and cut-out speed, and power vs. wind curve. The wind speed is defined for a reference height and the corresponding height and air density corrections are applied. As the PV generator, the wind generator also has a minimum generated power, which is defined as a percentage of the rated power.

ES Unit: It is a generic technology-independent model defined by its rated power, rated energy, minimum stored energy, efficiency (which is a function of ES loading) and a minimum charge/discharge power (defined as a percentage of the ES rated power); see [10,15]. Moreover, the model automatically sets a maximum charge/discharge power based on the stored energy and the simulation time-step.

Table 1. Parameters of a virtual power plant.

PV Generator	Energy Storage Unit
<ul style="list-style-type: none"> • Rated power (kW) • Irradiance (kW/m²) • Power vs. Temperature curve • Panel temperature (°C) • Minimum power (%) • Power curtailment (%) 	<ul style="list-style-type: none"> • Rated power (kW) • Rated energy (kWh) • Minimum stored energy (kWh) • Efficiency curve • Minimum power (%)
Wind Generator	Inverter
<ul style="list-style-type: none"> • Rated power (kW) • Wind speed (m/s) • Hub height (m) • Cut-in speed (m/s) • Cut-out speed (m/s) • Power vs. Wind speed curve • Wind Reference height (m) • Altitude over sea-level (m) • Roughness length in wind direction (m) • Ambient temperature (°C) • Power curtailment (%) 	<ul style="list-style-type: none"> • Rated power (kVA) • Rated voltage (kV) • Power factor • Efficiency curve • Minimum power (%) • No-load power (%) • Number of phases • Connection (delta/wye) • ZIP coefficients

Inverter: The inverter acts as a bridge between the DC network, to which the GU and ES unit are connected, and the AC distribution system; it allows a bidirectional power flow between the VPP and the grid. The inverter only absorbs/injects power if the power on the AC-side is greater than the predefined minimum power (defined as a percentage of the inverter rated power). The efficiency curve is defined as a function of the power output (in kVA) with respect to the inverter rated power. The absorbed power during the idle conditions (i.e. no active power output) is determined by the No-load power value. The idle power consumed by the VPP depends on the passive elements (e.g. filters and transformers) and the necessary power to operate the DC network; this power is defined in the model as a percentage of the inverter rated power and modeled as a ZIP load. The ZIP load model is constructed as a combination of constant power, constant current and constant impedance load models [16]; ZIP coefficients are defined in the following order:

$$ZIP \text{ coefficients} = [C_Z, C_I, C_P] \quad (1)$$

where C_Z is the weight assigned to the constant impedance load model, C_I is assigned to the constant current model, and C_P is the weight that represents the portion of the load modeled as constant power.

The inverter is also responsible for providing the required reactive power, being the maximum reactive power that the inverter can inject/absorb determined by the user-defined power factor (PF) parameter:

$$Q_{max} = kVA_{RATED} \sqrt{1 - PF^2} \quad (2)$$

The provided reactive power will have an effect on the inverter efficiency; this effect will be included, using the same approach presented in [17], as follows:

$$\eta(s, pf) = f(s) \cdot \alpha(pf) \quad (3)$$

$$s = \frac{kVA}{kVA_{RATED}} \quad (4)$$

$$\alpha(pf) = 0.98 + 0.02 \cdot pf \quad (5)$$

where Q_{max} is the maximum reactive power and kVA_{RATED} is the inverter rated power. η is the efficiency curve for any load level, s , and any output power factor, pf , $f(s)$ is the efficiency curve for a unity power factor, which depends on the load level (measured at the AC-side), and α is a scale factor that depends on the power factor.

2.3. VPP operation

The VPP model has been developed for time-driven simulations and takes advantage of OpenDSS built-in capabilities (i.e. loadshapes, linear interpolation, complex number operations, etc.). Two operation modes have been defined for the VPP: (i) Follow mode; (ii) Dispatch mode.

2.3.1. Follow operation mode

Under this operation mode the ES unit and the GU behave according to the curve shapes assigned to each component. The PV generator requires curves describing the solar irradiance and panel temperature for the evaluation period, while the wind generator follows the curves that define the wind speed (measured at a reference height) and the ambient temperature. On the other hand, ES unit operates according to a curve that defines the charge and discharge states, as well as the absorbed and injected power. The reactive power provided by the inverter is equal to the maximum reactive power times the corresponding multiplier stored in a user-defined curve shape.

The total VPP power output is not controlled and depends on the power resulting from the interaction between the GU and the ES unit. The model follows the same convention as the OpenDSS Storage object: Negative values correspond to power absorption, while power injection is defined by positive values. The VPP powers are calculated according to the following equations (see Figure 1):

$$P_{IN} = P_{DG} + P_{ES} \quad (6)$$

$$P_{OUT} = \begin{cases} \eta \cdot P_{IN}, & P_{OUT} \geq 0 \\ \frac{P_{IN}}{\eta}, & P_{OUT} < 0 \end{cases} \quad (7)$$

where P_{DG} is the power produced by the GU, P_{ES} is the power provided by the ES unit, P_{IN} is the power measured at the inverter DC-side, P_{OUT} is the active power measured at the inverter AC-side, and η is the inverter efficiency, calculated according to Equations (3) through (5).

2.3.2. Dispatch operation mode

Under this operation mode, the VPP is required to follow a dispatch curve that defines the active and reactive power output for each time-step during the evaluation period. The objective is to fully utilize the capacity of the renewable resource, so ES operation will be subjected to the lack or excess of renewable generation. Additionally, the VPP can draw power from the grid in order to charge the ES unit. The complete operation strategy is depicted in Figure 2; note that Equations (6) and (7) remain valid.

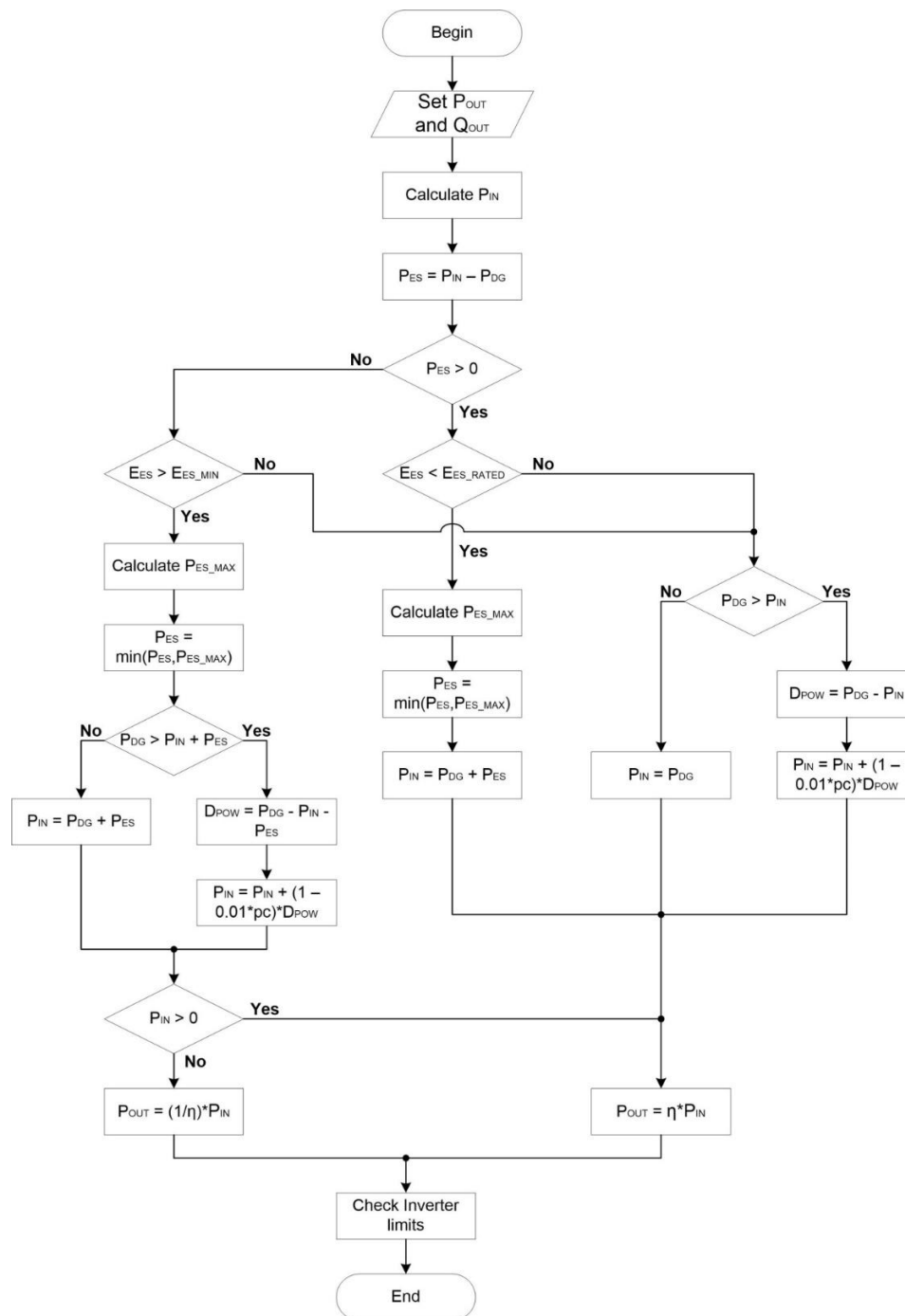


Figure 2. Dispatch operation mode.

In Figure 2 E_{ES} is the current stored energy in the ES unit, E_{ES_RATED} is the ES rated energy, E_{ES_MIN} is the minimum stored energy, P_{ES_MAX} is the maximum power the ES unit can absorb/inject based on the current stored energy, and pc is the power curtailment parameter.

The following aspects must be taken into account for the Dispatch operation mode:

- P_{OUT} is calculated as the inverter rated power times the corresponding multiplier stored in a user-defined curve shape.
- The reactive power provided by the inverter (Q_{OUT}) is equal to the maximum reactive power times the corresponding multiplier stored in a user-defined curve shape.
- P_{IN} is calculated from Equation (7).
- The power produced by the GU is defined by the curves describing the renewable resource (irradiance or wind speed) and temperature (panel or ambient) for the evaluation period.
- The ES unit main task is to compensate for the lack or excess of renewable generation. ES power will be adjusted so P_{IN} matches the power required to meet the VPP dispatch.
- By defining a negative multiplier, the VPP can be forced to absorb active power, which will be used to charge the ES unit with power coming from the distribution network.
- VPP operation is meant to follow the power dispatch as accurately as possible; therefore, renewable generation may be curtailed in order to prevent any deviation from the dispatched power. For example, assume the ES unit is fully charged and the available power is greater than the required power to meet the VPP dispatch; under this condition, the GU production will be reduced in order to match the dispatched power. However, power curtailment is not a binary decision, that is, the amount of power to be curtailed is defined by the power curtailment parameter.
- If the available power in the VPP (including ES and GU) is not enough to meet the dispatched power, the VPP will export as much power as resource availability allows.
- The VPP can enter an idle state under three conditions: (i) the dispatched active power is equal to zero; (ii) the available power within the VPP is zero, which would make the VPP unable to meet any dispatched power, and (iii) S_{OUT} (the apparent power at the AC-side) is smaller than the inverter minimum power. In idle state the VPP will only draw active power, determined by the user-defined No-load parameter and ZIP coefficients.
- The last step in the procedure verifies that S_{OUT} is not greater than the inverter rated power; if so, the model will adjust P_{OUT} , Q_{OUT} , P_{DG} , and P_{ES} so the resulting S_{OUT} is equal to the inverter rated power. This function is also used under the Follow operation mode.
- For a time-driven simulation, the procedure must be repeated for every time-step.

3. Simulation of the VPP Model Under Dispatch Operation Mode

3.1. Test system configuration and characteristics

This section is aimed at illustrating the behavior of the VPP model running under Dispatch operation mode. Figure 3 shows the test system: it is a three-phase 60-Hz overhead system serving two spot loads supplied from a HV/MV substation transformer. The VPP is connected to the MV network through a distribution MV/LV transformer.

The main characteristics of the test system are as follows:

- HV rated voltage: 230 kV

- MV rated voltage: 4.16 kV
- LV rated voltage: 0.4 kV
- Substation transformer rated power: 500 kVA
- MV/LV transformer rated power: 210 kVA.

System loads have been modeled as voltage-independent. Load profiles, solar irradiance, wind speed, and panel and ambient temperature curves were derived with the procedure presented in [14]. The actual voltage at the substation HV terminals is 1.05 pu.

The main characteristics of the VPP are presented in Table 2; the study will consider both the Solar and Wind VPP. The efficiency curves used for the inverter and ES unit are shown in Figures 4 and 5, the power vs. Temperature curve of the PV generator is presented in Figure 6, and the power vs. wind speed curve is shown in Figure 7.

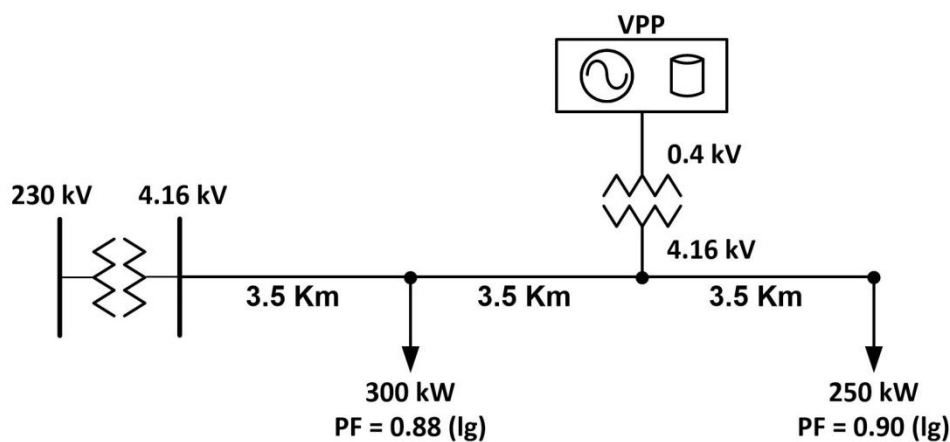


Figure 3. Case study 1: Test system configuration.

Table 2. Case study 1: VPP characteristics.

PV Generator	Energy Storage Unit
Rated power: 200 kW	Rated power: 200 kW
Minimum power: 5%	Rated energy: 2000 kWh
Power curtailment: 100%	Initial stored energy: 1000 kWh
	Minimum stored energy: 400 kWh
	Minimum power: 5%
Wind Generator	Inverter
Rated power: 200 kW	Rated power: 200 kVA
Hub height: 35 m	Rated voltage: 0.4 kV
Cut-in speed: 4 m/s	Power factor: 0.9
Cut-out speed: 20 m/s	Minimum power: 5%
Wind Reference height: 50 m	No-load power: 1%
Altitude over sea-level: 64 m	Number of phases: 3
Roughness length in wind direction: 0.8 m	Connection: delta
Minimum power: 2.4%	ZIP coefficients: [0.9, 0, 0.1]
Power curtailment: 100%	

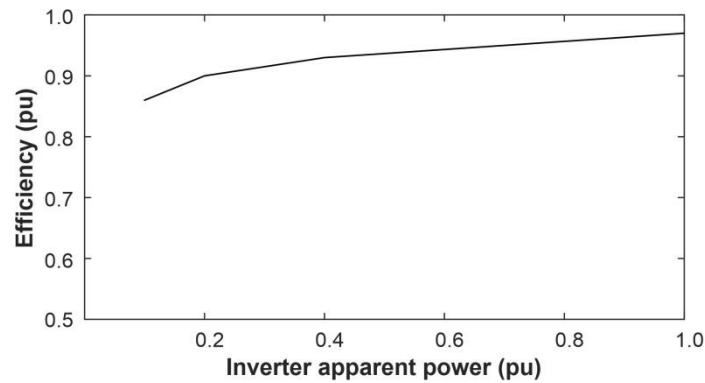


Figure 4. Case study 1: Inverter efficiency curve.

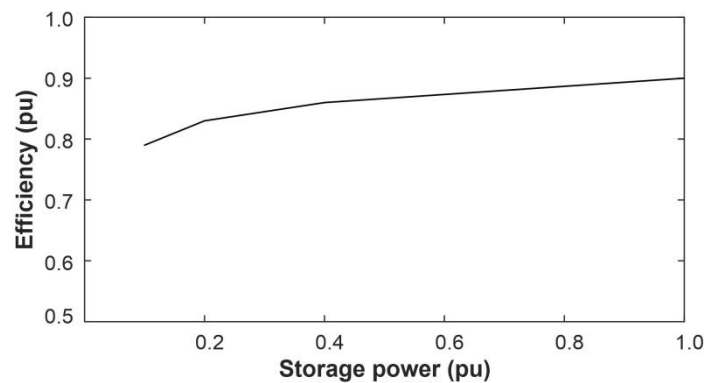


Figure 5. Case study 1: ES unit efficiency curve.

3.2. Simulation results

The test system has been simulated for a period of 24 hours with a 1-hour time-step and system curves generated for a 1-year period. The selected 24 hours belong to a specific day of the year. Five different scenarios have been considered for simulation:

- (1) system without VPP (i.e. without DG and ES), also referred to as base case;
- (2) system with PV generation only;
- (3) system with Solar VPP;
- (4) system with only wind generation;
- (5) system with Wind VPP.

The day under consideration presents distinctive variations between high and low load conditions (see Figure 8a); moreover, there is no significant correlation between system load and renewable resources, which will help to accentuate the advantages of a VPP with respect to DG without ES. Note that the load curves for the previous and following day present different values and characteristics.

Figure 8b depicts the load voltages for the base case. For Scenarios 3 and 5, the VPPs operate under the Dispatch operation mode and follow the dispatch curve depicted in Figure 9. Take into account that the dispatch curve has not been optimized and no reactive power is dispatched in these scenarios. The operating conditions resulting from all scenarios are shown in Table 3.

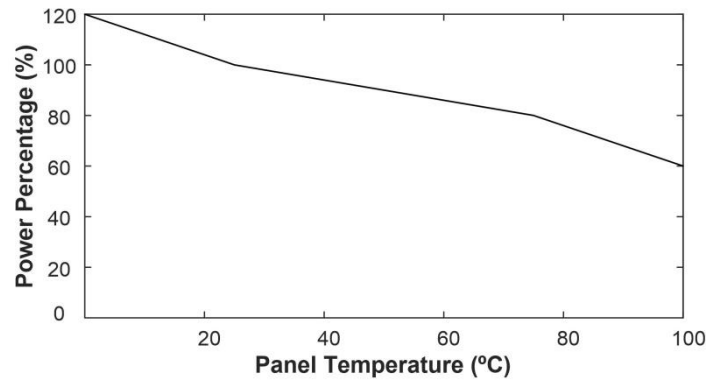


Figure 6. Case study 1: Power vs. temperature curve.

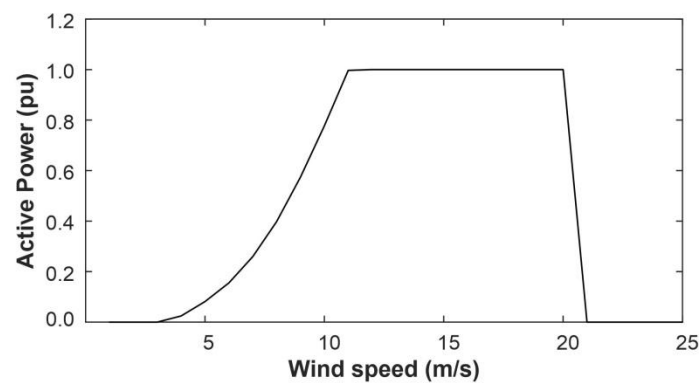


Figure 7. Case study 1: Power vs. wind speed curve.

Figure 10 depicts the active power measured at the MV-side of the substation transformer. As expected, there is a reduction in the active energy supplied by the substation transformer in Scenarios 2 through 5; moreover, all these scenarios also produced improvements in peak power and minimum voltage (see Figures 10 and 11). This is due to the fact that the peak load occurs in the morning when PV and wind generation are non-zero; however, there is a second peak at nighttime, on which DG without ES has little or no effect.

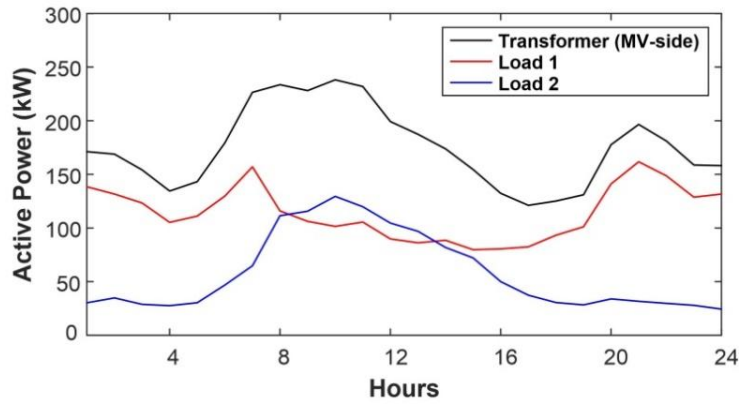
Another important aspect is the effect of the intermittent nature of the solar and wind generation: in Scenarios 2 and 4 DG is allowed to produce as much energy as possible, but due to the low correlation between generation and load, too high system voltages are produced.

The VPPs were capable of producing a greater impact on the operating conditions as both can adjust the power output according to the load behavior. The resulting active power and load voltage profiles present a much flatter behavior than the other scenarios (see Figures 10 and 11).

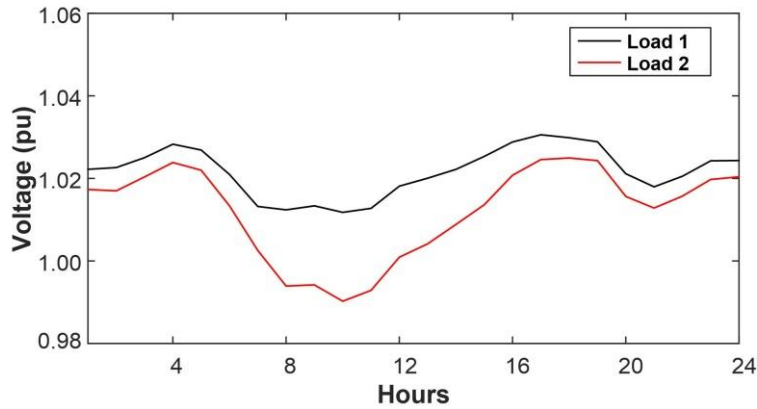
The VPP dispatch curve was designed to mirror the behavior of the active power curve in the base case; consequently, the VPP power output is a reflection of the system's state and undesired conditions are avoided (e.g. too high system voltages).

For the present case study, the Wind VPP was capable of following the dispatch curve without any deviations, whereas the Solar VPP failed to meet the dispatched power at the 9th and 10th hours, see Figure 12. The solar irradiance curve and the demanded power in the early hours of the day, forced the Solar VPP to depend entirely on the energy stored in the ES unit; by the 8th hour the stored energy had reached its minimum value and the power produced by the PV generator was not

enough to meet the dispatch curve. As of the 11th hour, the power produced by the PV generator was sufficient to satisfy the dispatched power and charge the ES unit for the upcoming night hours; the operation curves of the VPP components are presented in Figure 13.



(a) Active power curves



(b) Load node voltage-Phase A

Figure 8. Case study 1: Base case.

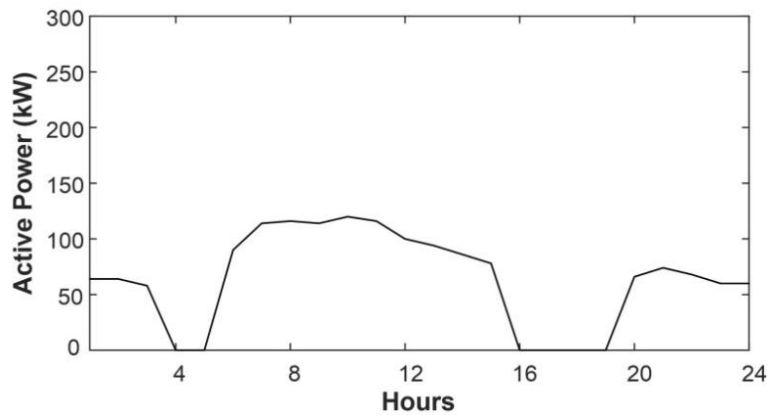


Figure 9. Case study 1: VPP dispatch curve.

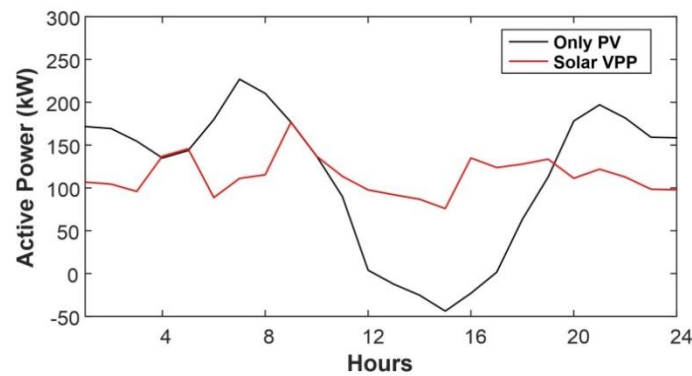
Table 3. Case study 1: Test system operating conditions.

	Base case	Only PV	Solar VPP	Only Wind	Wind VPP
Active energy served (kWh) ¹	4206.1	2851.7	2747.4	2852.9	2661.1
Reverse energy flow (kWh) ¹	-	-104.4	0.0	-64.4	0.0
Energy losses (kWh) ²	76.5	80.5	62.0	76.2	60.9
Maximum active power (kW) ¹	238.1	226.9	176.7	213.9	145.8
Minimum active power (kW) ¹	121.1	-43.8	75.9	-49.1	75.9
Maximum voltage (pu)	1.0500	1.0556	1.0500	1.0593	1.0500
Minimum voltage (pu)	0.9902	0.9971	1.0017	0.9953	1.0083
DG/VPP energy (kWh) ³	-	1462.9	1444.3	1417.2	1529.4

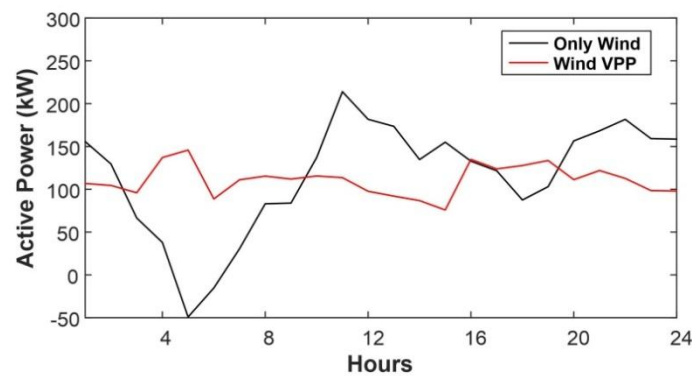
¹ Measured at the MV-side of the substation transformer.

² Measured losses do not include losses in the substation transformer.

³ Measured at the LV-side of the interconnection transformer.



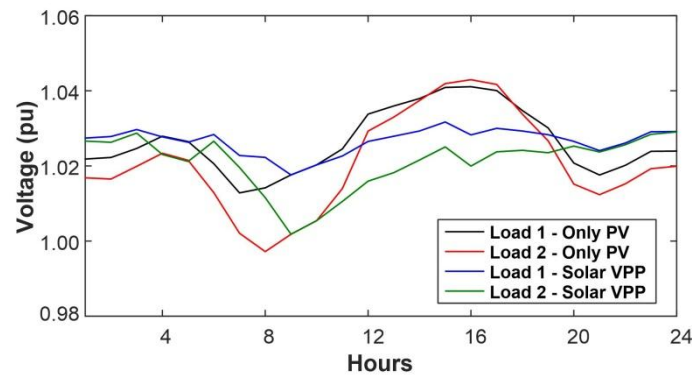
(a) Scenarios 2 and 3



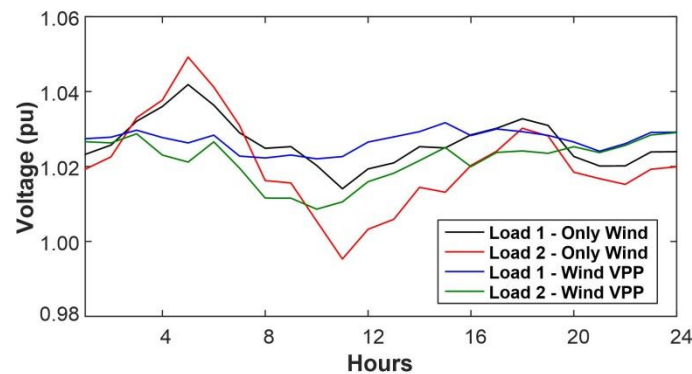
(b) Scenarios 4 and 5

Figure 10. Case study 1: Active power curves measured at MV-side substation terminals.

On the other hand, the wind profile allowed the Wind VPP to charge the ES unit with enough energy to meet the prescheduled power output for the entire day. Note that the wind generation in the second half of the day is much lower when compared to that in the first half; however, the proper operation of the VPP permitted to store this excess of energy so it could be released when it was required later on.



(a) Scenarios 2 and 3



(b) Scenarios 4 and 5

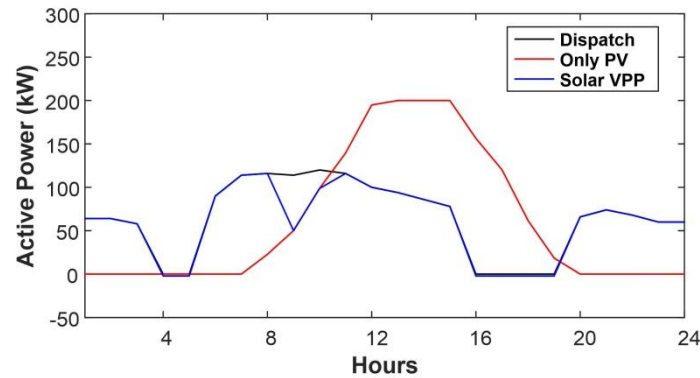
Figure 11. Case study 1: Load node voltages-Phase A.

The VPP operates under the idle state in two different periods, as determined by the dispatch curve. Information related to these time periods is presented in Table 4; it can be observed that the power absorbed by the VPP is not constant due to the voltage dependency of the VPP ZIP load model. It is worth noting that when GU production is non-zero, the entirety of this power is used to charge the ES unit. Another important aspect is that a power curtailment is carried out in the Wind VPP at the 5th hour; due to the different corrections, the wind generated power is slightly greater than the GU rated power (201.3 kW). However, the ES unit can absorb a maximum power of 200 kW; as a consequence, the wind power was curtailed to meet the ES unit requirements.

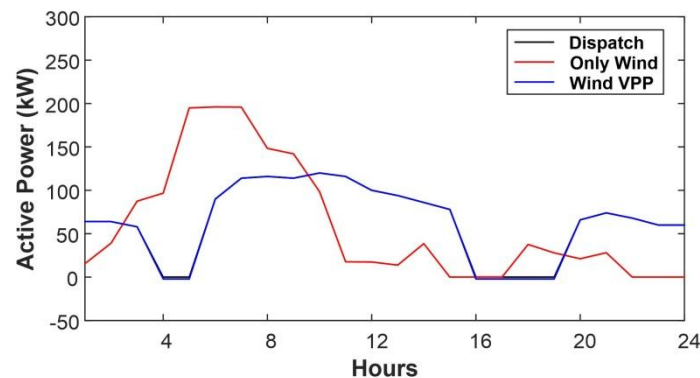
4. Day-Ahead Dispatch Optimization

4.1. Optimization procedure

The dispatch curve used in the previous section was not derived by means of any optimization procedure; however, in order to maximize the potential benefits to the distribution system it is necessary for the VPP to follow a curve that has been optimized for the evaluation period under consideration. The VPP operation can be conducted from the perspective of a utility (i.e. aiming to improve network conditions) or operated by a private operator (i.e. with the objective of generating profits). The VPP dispatch optimization can be implemented following an approach similar to those used for determining the optimum operation of ES (e.g. [18–27]).



(a) Scenarios 2 and 3



(b) Scenarios 4 and 5

Figure 12. Case study 1: Active power output.

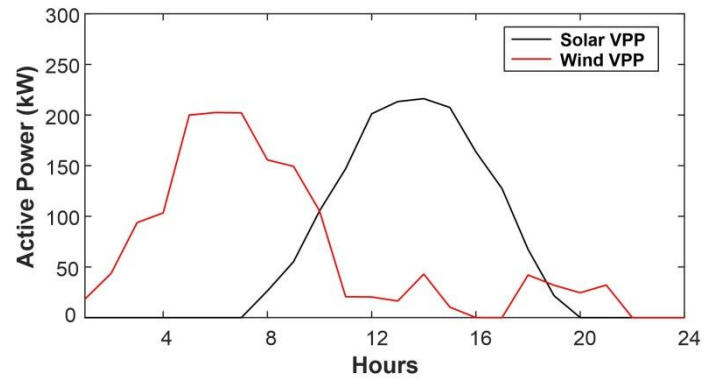
Day-ahead dispatch is based on the system's forecast for the following day; the VPP operation must be optimized according to these forecasted load and renewable resource curves. This section presents a procedure for determining the optimal hourly day-ahead dispatch of multiple VPPs from the utility's perspective.

In this section the VPP optimal dispatch is determined by means of a general parallel genetic algorithm (GPGA). The implemented GPGA is a global single-population GA [28], where only one population is created and the evaluation of each member of a given generation is independent from the rest of the members; therefore, the evaluation of a generation can be seen as an embarrassingly parallel problem [29]. This approach yields a reduction of the total execution times by distributing the evaluation of individuals in a generation among available cores in a multi-core installation.

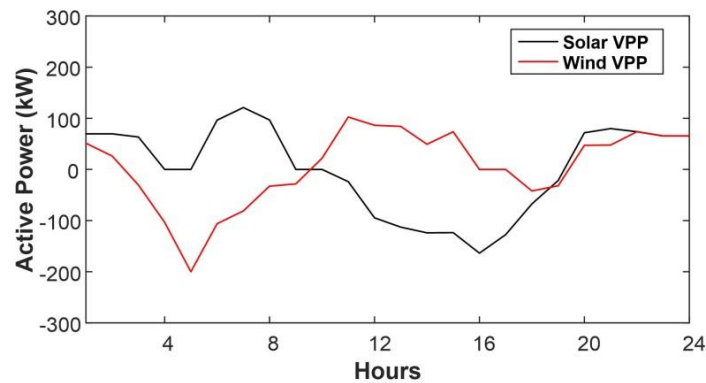
The GPGA will seek to determine the optimal values for every point of the VPP operation curve that minimize the following operation variables:

- Distribution energy losses, without including losses in substation transformer (EL).
- Energy supplied from the MV-side of the substation transformer (E).
- Peak power supplied by the substation transformer from the MV-side terminals (P_{MAX}).

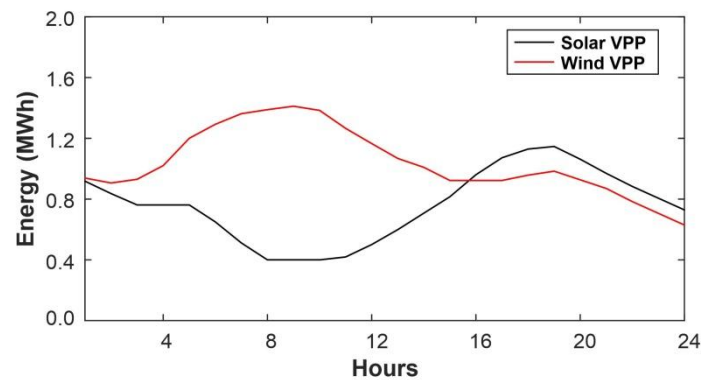
For a day-ahead dispatch with a 1-hour time step, the VPP operation curve will consist of 24 values, which can be either positive or negative (according to the power injection or absorption). Note that the procedure can cope with multiple dispatch curves; that is, different VPPs can follow different operation curves. The parameters used in the optimization procedure are shown in Table 5.



(a) GU power curve



(b) ES unit power curve



(c) ES unit energy curve

Figure 13. Case study 1: VPP components operation curves.**Table 4.** Case study 1: VPP idle state.

Hour	Dispatched P_{OUT}	Solar VPP			Wind VPP		
		Idle P_{OUT}	P_{DG}	P_{ES}	Idle P_{OUT}	P_{DG}	P_{ES}
4	0.0	2.0913	0.0	0.0	2.0913	103.4	-103.4
5	0.0	2.0855	0.0	0.0	2.0853	200.0	-200.0
16	0.0	2.0867	163.6	-163.6	2.0867	0.0	0.0
17	0.0	2.0968	127.4	-127.4	2.0968	0.0	0.0
18	0.0	2.0962	67.3	-67.3	2.0963	42.1	-42.1
19	0.0	2.0933	21.5	-21.5	2.0933	31.9	-31.9

Two stopping criteria have been established for the optimization procedure:

- (1) The generation count (i.e. the number of executed generations) is equal to the established maximum number of generations.
- (2) The best fitness changes less than ε over δ generations.

The GPGA has been implemented in MATLAB and the evaluation of each member in a population is conducted by simulating the test system during one day using a 1-hour time-step. Individual executions are distributed among 4 cores using the library developed by M. Buehren [30]. The procedure was tested on a laptop computer with an Intel Core i7-6700HQ processor (4 Cores, Clock frequency = 2.6–3.5 GHz), 12 GB RAM, and Windows 10 OS.

Table 5. Case study 2: GPGA parameters.

Maximum number of generations	200
Number of traits	24 × Number of dispatch curves
Population size	10 × Number of traits
Epsilon (ε)-Tolerance	0.0001
Delta (δ)-Number of generations for best fitness checking	20
Crossover probability (p_c)	0.80
Mutation probability (p_m)	0.02
Elitism	Yes
Maximum curve value ¹	1.00
Minimum curve value ¹	-1.00

¹ It is a factor of the VPP inverter rated power.

The fitness function calculated for every evaluation will be equal to the square root of the sum obtained from the operation variables:

$$Fitness = \sqrt{\left(\frac{E_{VPP}}{E_{BASE}}\right)^2 + \left(\frac{EL_{VPP}}{EL_{BASE}}\right)^2 + \left(\frac{P_{MAX_VPP}}{P_{MAX_BASE}}\right)^2 + (\Delta R_{PF})^2 + \sum_{i=1}^{N_{VPP}} \Delta E_i^2 + \sum_{i=1}^{N_{VPP}} CD_i^2} \quad (8)$$

$$\Delta R_{PF} = \begin{cases} 0, P_{MIN_VPP} > 0 \\ \frac{P_{MIN_VPP}}{P_{MAX_BASE}}, P_{MIN_VPP} \leq 0 \end{cases} \quad (9)$$

$$\Delta E = \begin{cases} 0, E_{ES_LIM-} \leq E_{ES} \leq E_{ES_LIM+} \\ \frac{E_{ES_OBJ} - E_{ES}}{E_{ES_OBJ}}, else \end{cases} \quad (10)$$

where N_{VPP} is the number of VPPs in the system, P_{MIN} is the minimum power served by the substation transformer from the MV-side; E_{ES_OBJ} is the expected stored energy in the ES unit at the end of the evaluation period; E_{ES_LIM-} and E_{ES_LIM+} are the lower and upper limits of a bandwidth around E_{ES_OBJ} ; CD is the Euclidean distance between the proposed dispatch curve and the actual VPP output curve. The sub index *BASE* makes reference to the base case (i.e. system without DG or VPP), while *VPP* is used for those quantities obtained when the VPPs are present in the system. ΔR_{PF}

has been introduced in the fitness function as penalty for those cases in which reverse power flow occurs, while ΔE is a penalty for those cases when the ES unit stored energy falls outside of the bandwidth defined by E_{ES_LIM-} and E_{ES_LIM+} . Forcing the ES unit to maintain a minimum value of stored energy at the end of the evaluation period will ensure that the VPP will have enough energy for meeting the following day's dispatch (i.e. the day after the day-ahead).

The procedure seeks to minimize the value of the fitness function presented in Equation (8). For every evaluation, the procedure checks that all voltages are within accepted limits (between 0.95 and 1.05 pu), no network element experiences overload, and the iterative algorithm converges for all solution steps. If one or more of these conditions are not fulfilled, the procedure will assign a large value to the fitness function, which will make difficult its participation in the subsequent generations of the GPGA.

4.2. Test system configuration

The new test system prepared for this case study is a three-phase 60-Hz overhead system with a simplified representation of the HV transmission system (see Figure 14). VPPs use the same configuration as in the previous test system, see Figures 3 through 7. By default, all distribution loads are connected to the system through MV/LV transformers.

Some important information related to the new test system follows:

- HV rated voltage: 230 kV.
- HV actual voltage: 1.03 pu.
- MV rated voltage: 4.16 kV.
- LV rated voltage: 0.4 kV.
- Substation transformer rated power: 2500 kVA.
- Total rated active load: 1700 kW.

As in Test System 1, loads have been modelled as voltage-independent and curve shapes have been derived with the procedure presented in [14].

Solar VPP 1 and Wind VPP 1 use the same parameters as those in case study 1; furthermore, the expected stored energy, and lower and upper bandwidth limits have been set to 1500, 800, and 1200 kWh, respectively. The characteristics of Solar VPP 2 and Wind VPP 2 are presented in Table 6 (all VPPs operate under the Dispatch operation mode). Note that the rated values and locations of all VPPs have been arbitrarily chosen. It is assumed that the solar irradiance and reference wind speed are the same for the entire system; due to height corrections the actual wind speed curve will be different for both Wind VPPs.

4.3. Simulation results

The GPGA was executed to obtain the optimal day-ahead dispatch of active power for the VPPs in the system. Due to the different nature of wind and solar resources, the procedure will derive two dispatch curves: the first one will be assigned to the Solar VPPs, while the Wind VPPs will operate according to the second dispatch curve. As in the previous study, the selected 24 hours belong to a specific day of the year, and the load curves for the previous and following day present different values and characteristics.

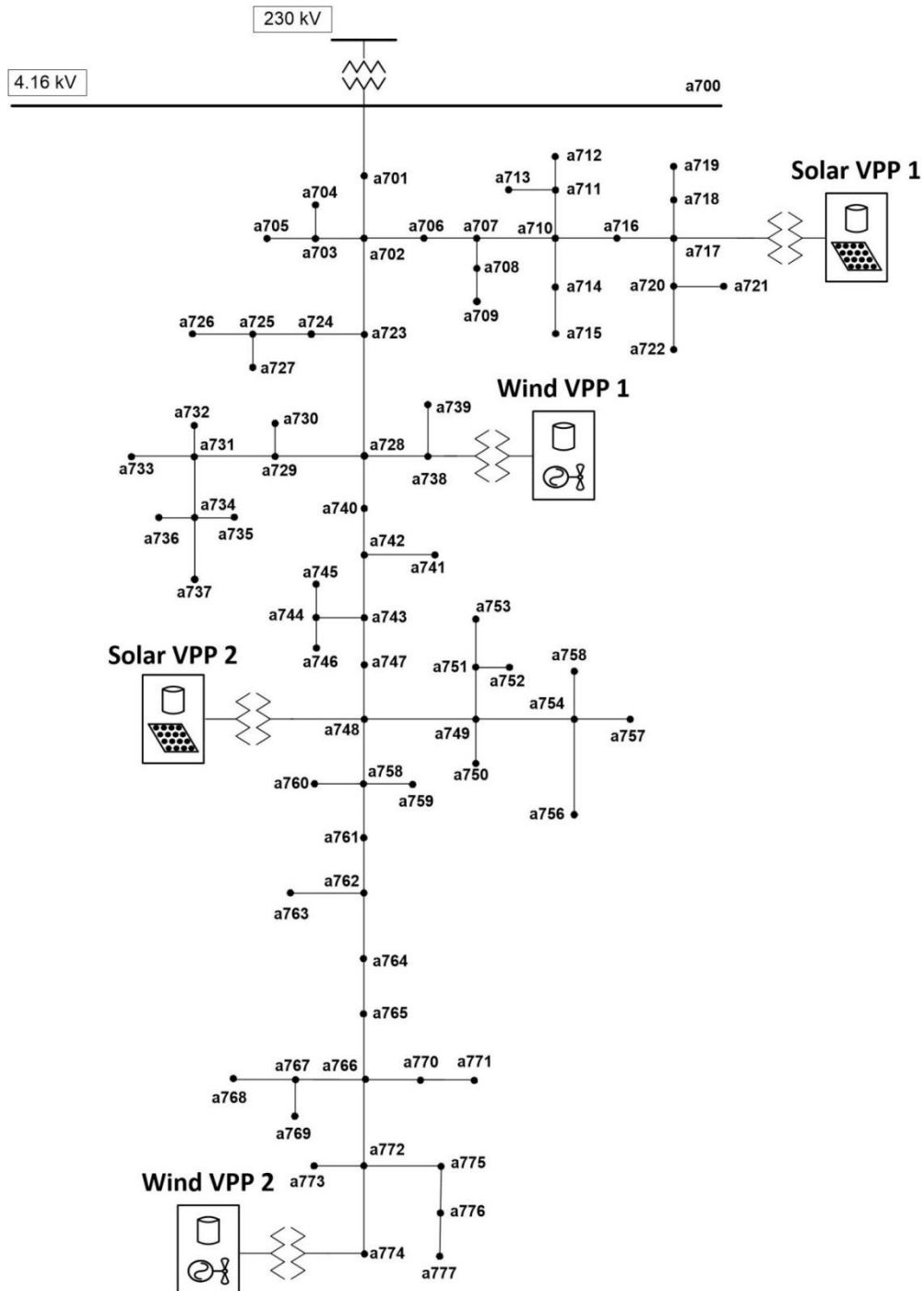


Figure 14. Case study 2: Test system configuration.

A GA is a stochastic optimization procedure; thus, it is possible for it to converge before reaching the optimum solution; therefore, two different scenarios have been considered for the GPGA execution:

- (1) the GPGA will consider both stopping criteria mentioned above;
- (2) the procedure is executed without the δ/ε criterion; that is, the procedure will stop when it has reached the maximum number of generations.

The results for both scenarios are presented in Table 7. The table also includes the operation variables for the base case. These results show a clear improvement on the energy and peak power served by the substation transformer; both operation variables (as well as the best fitness) present consistent values for both scenarios. On the other hand, it was not possible to produce a reduction on the energy losses; however, the energy losses for the base case do not include the losses of the VPP interconnection transformers, which represent a new and significant source of losses; energy losses including only the interconnection transformers amount to 618.4 kWh.

Table 6. Case study 2: VPP characteristics.

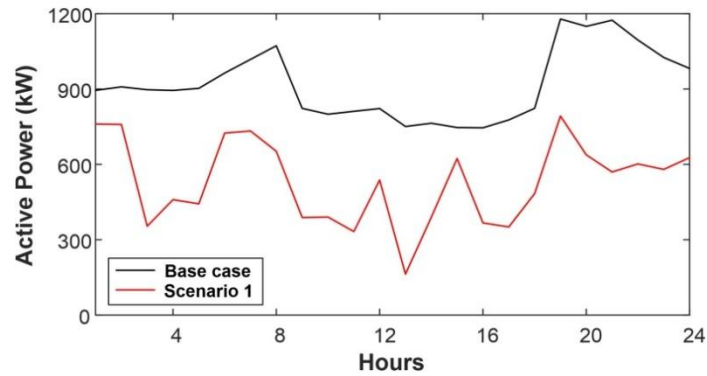
Solar VPP 2		
PV Generator	Energy Storage Unit	Inverter
Rated power: 300 kW	Rated power: 300 kW	Rated power: 300 kVA
Minimum power: 5%	Rated energy: 3000 kWh	Rated voltage: 0.4 kV
Power curtailment: 100%	Initial stored energy: 1500 kWh	Power factor: 0.9
	Minimum stored energy: 600 kWh	Minimum power: 5%
	Minimum power: 5%	No-load power: 1%
	Expected stored energy: 1500 kWh	Number of phases: 3
	Lower limit: 1200 kWh	Connection: delta
	Upper limit: 1800 kWh	ZIP coefficients: [0.9, 0, 0.1]
Wind VPP 2		
Wind Generator	Energy Storage Unit	Inverter
Rated power: 300 kW	Rated power: 300 kW	Rated power: 300 kVA
Hub height: 45 m	Rated energy: 3000 kWh	Rated voltage: 0.4 kV
Cut-in speed: 4 m/s	Initial stored energy: 1500 kWh	Power factor: 0.9
Cut-out speed: 20 m/s	Minimum stored energy: 600 kWh	Minimum power: 5%
Wind Reference height: 50 m	Minimum power: 5%	No-load power: 1%
Altitude over sea-level: 64 m	Expected stored energy: 1500 kWh	Number of phases: 3
Roughness length: 0.8 m	Lower limit: 1200 kWh	Connection: delta
Minimum power: 2.4%	Upper limit: 1800 kWh	ZIP coefficients: [0.9, 0, 0.1]
Power curtailment: 100%		

Table 7. Case study 2: Simulation results.

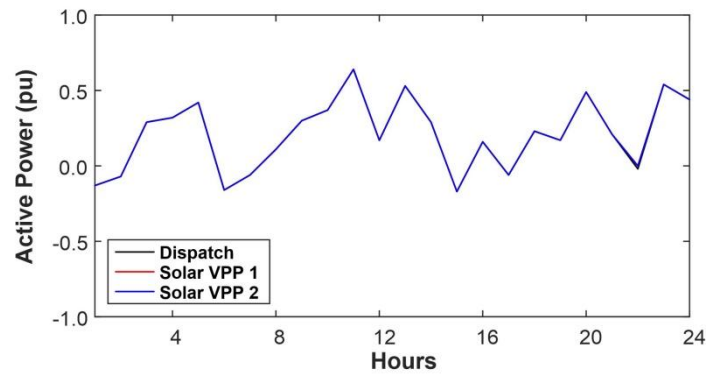
	Base case	Scenario 1	Scenario 2
Best fitness	-	1.3827	1.3765
Generation count	-	57	200
Simulation time (sec)	-	501.7	1625.0
Energy (kWh)	22021.2	12722.6	12753.5
Energy losses (kWh)	566.6	583.4	589.4
Maximum power (kW)	1178.9	792.4	752.7
Stored energy Solar VPP 1 (kWh) ¹	-	828.4	808.4
Stored energy Solar VPP 2 (kWh) ¹	-	1242.6	1212.6
Stored energy Wind VPP 1 (kWh) ¹	-	744.7	764.7
Stored energy Wind VPP 2 (kWh) ¹	-	1763.9	1779.9

¹ Measured at the end of the evaluation period.

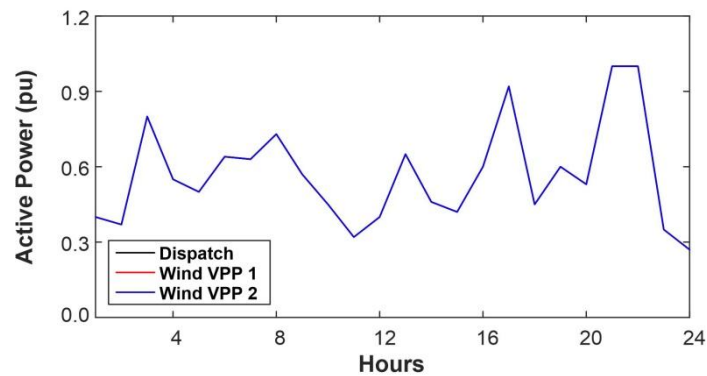
Figure 15 depicts the active power profile for the base case and the resulting profile from Scenario 1; additionally, it presents the obtained dispatch curves and the actual VPP operation curve. Figure 15a shows that the VPP operation produced a sustained reduction on the active power served from the substation transformer, while Figures 15b and 15c demonstrate that the VPPs are capable of accurately following their dispatch curves.



(a) Active power profile



(b) Solar VPP dispatch



(c) Wind VPP dispatch

Figure 15. Case study 2: Simulation results.

The only deviation present in the VPP dispatch occurs for the Solar VPP; the dispatch curve set a charging power of -0.02 pu at the 22nd hour; however, this value is smaller than the inverter minimum power, which forces the VPP to enter the idle state. It is important to observe that both

dispatch curves present different behaviors throughout the evaluation period, which is likely to be caused by the different nature of both resources.

Due to difference in hub height, the Wind VPP 2 will produce more power and energy (in pu) than the Wind VPP 1; as a result, the stored energy in the ES unit at the end of the evaluation period (with respect to the rated energy) will also be greater, see Table 7. In general, the stored energy in the Wind VPP 2 at the end of the evaluation period is always close to the bandwidth's upper limit, which means that the VPP could inject more energy into the system and still remain within the desired bandwidth; however, the Wind VPP 2 cannot use this extra energy if it is forced to follow the same dispatch curve as the Wind VPP 1. In order to explore the possibility of utilizing the extra energy stored in the Wind VPP 2, the GPGA has been executed considering one dispatch curve for each Wind VPP. Additionally, the GPGA was also executed considering one dispatch curve per VPP (i.e. 4 dispatch curves). Simulation results for these new conditions are presented in Table 8.

Results in Table 8 show that by defining a dispatch curve for each Wind VPP (i.e. 3 dispatch curves) a slight improvement in the energy and maximum power served by the substation transformer has been produced; moreover, it allowed the Wind VPP 2 to inject as much energy as possible into the system (while respecting the stored energy bandwidth). On the other hand, using one dispatch curve per VPP (i.e. 4 dispatch curves) produced no improvement with respect to the previous executions of the optimization procedure.

Tables 7 and 8 show that Scenario 2 produced better results than Scenario 1 (in terms of best fitness values), although the operation variables present low variations; moreover, using 3 dispatch curves produced the best results among all executions. This behavior indicates that VPPs with different characteristics and GU output (in pu) can be operated using individual dispatch curves.

Simulation times have been affordable for all GPGA executions, ranging from 5 minutes to 1 hour; these times vary according to the number of executed generations and population size, which is a function of the number of dispatch curves to be optimized (see Table 5).

Table 8. Case study 2: Simulation results-Multiple dispatch curves.

	3 Dispatch curves ¹		4 Dispatch curves ²	
	Scenario 1	Scenario 2	Scenario 1	Scenario 2
Best fitness	1.3646	1.3233	1.3936	1.3999
Generation count	52	200	23	200
Simulation time (sec)	680.8	2547.9	364.9	3382.1
Energy (kWh)	12696.1	12461.8	12941.9	12800.4
Energy losses (kWh)	596.7	584.5	596.2	622.4
Maximum power (kW)	758.9	711.3	803.8	757.1
Stored energy Solar VPP 1 (kWh) ¹	860.4	827.8	802.3	840.7
Stored energy Solar VPP 2 (kWh) ¹	1290.5	1241.7	1762.4	1211.5
Stored energy Wind VPP 1 (kWh) ¹	832.3	890.2	964.2	860.9
Stored energy Wind VPP 2 (kWh) ¹	1425.8	1288.7	1215.3	1301.9

¹ One dispatch curve per Wind VPP.

² One dispatch curve per VPP (Solar and Wind).

5. Conclusions

This paper has presented a virtual power plant model for power flow calculations. The model has been compiled as a custom-made capability within the OpenDSS COM DLL and can be used in time-driven simulations controlled from other software platforms, e.g. MATLAB. The model has the same capabilities as other OpenDSS objects and it can be defined, modified, and accessed using the same methods.

Two different operation modes have been implemented inside the model: Follow and Dispatch. Under the Follow mode the model behaves according to the curves assigned to the GU and ES unit, whereas in Dispatch mode the VPP acts as a dispatchable unit.

The list of features implemented in the model includes: (i) active and reactive power dispatch, (ii) power curtailment, (iii) inverter idle power modeled as a ZIP load, (iv) minimum power limit for GU and ES unit, (v) automatic calculation of ES unit maximum charge/discharge power, and (vi) inverter power limits.

The first case study has shown how the VPP can make better use of the renewable resources, since it is capable of storing the generation surplus and injecting it into the network during low generation periods; the presence of ES is essential for meeting the power dispatch curve.

Contrary to DG based only on intermittent resources, the VPP output can be adjusted to meet the system requirements and thus avoid undesired operating conditions, such as system voltages above accepted limits. This is a vital feature for achieving larger penetration factors of renewable generation without compromising normal system operation.

The VPP can help to further improve system operating conditions by injecting or absorbing reactive power; the absorption of reactive power is expected to play a key role if the objective is to export energy to the transmission system [31].

The paper has also presented a procedure for determining the optimal day-ahead dispatch for the VPP based on a GPGA. The procedure seeks to explore the potential improvement on the overall operating conditions when the VPP is operated from the perspective of a utility. The presented methodology relies on a power flow simulator (i.e. OpenDSS) for calculating the system operating conditions; namely, no simplifications are introduced into the solution of the electrical system. Furthermore, the evaluated system can be of any size and include detailed models and control algorithms for system components (e.g. the presented VPP model). An accurate calculation of system conditions is essential for the optimization methodology since a poor estimation would cause the procedure to produce erroneous results.

A genetic algorithm requires a large number of executions in order to produce accurate results; although each individual execution does not require large simulation times, the repeated evaluation of the system could result in prohibitive executions times if they were to be performed in a sequential manner (i.e. using single core computing). This work makes use of parallel computing in combination with the GA (i.e. a GPGA) in order to distribute the individual executions among the available cores to produce a reduction in the total execution times.

The results presented in the second case study show that the proposed optimization procedure is capable of producing significant improvements on the system conditions and that the parallel approach used in this work produces affordable simulation times. These simulation times could be further reduced through the use of a larger multi-core installation.

Similar results to those presented in this paper could be achieved by defining appropriate operation curves of an OpenDSS Storage object that works in conjunction with the PV System or Generator objects; however, the coordination between both objects should be handled by an external tool (e.g. MATLAB), which would represent a significant loss in performance. The main advantage of the present model is that all operations and control decisions are compiled within the COM DLL, which makes them seamless to the user and helps to maintain the high computing performance of OpenDSS.

In its present form the developed VPP model is adequate for exploring the effect that the aggregation of renewable generation and energy storage can have on the system. Future work could be aimed at expanding the VPP model to incorporate losses in the DC network and implement an algorithm to automatically control the inverter's reactive power based on the system's conditions. Furthermore, an optimization procedure must be implemented in order to determine the optimal VPP operation curve for an extended evaluation period (i.e. one year or more).

Conflict of Interest

The author declares no conflicts of interest in this paper.

References

1. Willis HL, Scott WG (2000) Distributed power generation. Planning and evaluation. CRC Press.
2. Ackermann T, Andersson G, Söder L (2001) Distributed generation: a definition. *Electr Pow Syst Res* 57: 195–204.
3. Mahmoud PHA, Huy PD, Ramachandaramurthy VK (2017) A review of the optimal allocation of distributed generation: objectives, constraints, methods, and algorithms. *Renew Sust Energ Rev* 75: 293–312.
4. Sandia National Laboratories and NRECA (2015) DOE/EPRI Electricity Storage Handbook.
5. Li X, Hui D, Lai X (2013) Battery energy storage station (BESS)-based smoothing control of photovoltaic (PV) and wind power generation fluctuations. *IEEE T Sustain Energ* 4: 464–473.
6. Grillo S, Marinelli M, Massucco S, et al. (2012) Optimal management strategy of a battery-based storage system to improve renewable energy integration in distribution networks. *IEEE T Smart Grid* 3: 950–958.
7. Katsanevakis M, Stewart RA, Lu J (2017) Aggregated applications and benefits of energy storage systems with application-specific control methods: a review. *Renew Sust Energ Rev* 75: 719–741.
8. Etherden N, Vyatkin V, Bollen MHJ (2016) Virtual power plant for grid services using IEC 61850. *IEEE T Ind Inform* 12: 437–447.
9. International Electrotechnical Commission (2011) Electrical Energy Storage. Available from: <https://www.mendeley.com/research-papers/electrical-energy-storage-white-paper-3/>.
10. Dugan RC (2016) Reference Guide. The Open Distribution System Simulator (OpenDSS). EPRI.
11. Pudjianto D, Ramsay C, Strbac G (2007) Virtual power plant and system integration of distributed energy resources. *Iet Renew Power Gen* 1: 10–16.
12. Ghavidel S, Li L, Aghaei J, et al. (2016) A review on the virtual power plant: Components and operation systems. IEEE International Conference on Power System Technology. IEEE, 1–6.

13. Kolenc M, Nemček P, Gutsch C, et al. (2017) Performance evaluation of a virtual power plant communication system providing ancillary services. *Electr Pow Syst Res* 149: 46–54.
14. Martínez-Velasco JA, Guerra G (2015) Analysis of large distribution networks with distributed energy resources. *Ingeniare* 23: 594–608.
15. Dugan RC, Taylor JA, Montenegro D (2017) Energy storage modeling for distribution planning. *IEEE T Ind Appl* 53: 954–962.
16. Chassin DP (2013) Electrical load modeling and simulation. In: Khaitan SK, Gupta A, editors, *High Performance Computing in Power and Energy Systems*, Berlin: Springer.
17. Guerra G, Martínez-Velasco JA (2017) A solid state transformer model for power flow calculations. *Int J Elec Power* 89: 40–51.
18. Farzin H, Fotuhi-Firuzabad M, Moeini-Aghtaie M (2017) A stochastic multi-objective framework for optimal scheduling of energy storage systems in microgrids. *IEEE T Smart Grid* 8: 117–127.
19. Levron Y, Shmilovitz D (2012) Power systems' optimal peak-shaving applying secondary storage. *Electr Pow Syst Res* 89: 80–84.
20. Jayasekara N, Wolfs P, Masoum MAS (2014) An optimal management strategy for distributed storages in distribution networks with high penetrations of PV. *Electr Pow Syst Res* 116: 147–157.
21. Meirinhos JL, Rua DE, Carvalho LM, et al. (2017) Multi-temporal optimal power flow for voltage control in MV networks using distributed energy resources. *Electr Pow Syst Res* 146: 25–32.
22. Hejazi H, Mohsenian-Rad H (2016) Energy storage planning in active distribution grids: a chance-constrained optimization with non-parametric probability functions. *IEEE T Smart Grid*: 1–13.
23. Silvestre MLD, Graditi G, Ippolito MG, et al. (2011) Robust multi-objective optimal dispatch of distributed energy resources in micro-grids. Power Tech, 2011 IEEE Trondheim. IEEE, 1–5.
24. Agamah SU, Ekonomou L (2016) Peak demand shaving and load-levelling using a combination of bin packing and subset sum algorithms for electrical energy storage system scheduling. *Iet Sci Meas Technol* 10: 477–484.
25. Qin J, Sevlian R, Varodayan D, et al. (2012) Optimal electric energy storage operation. 2012 IEEE Power and Energy Society General Meeting, 1–6.
26. Pandzic H, Kuzle I (2015) Energy storage operation in the day-ahead electricity market. European Energy Market. IEEE, 1–6.
27. Lazaroiu GC, Dumbrava V, Balaban G, et al. (2016) Stochastic optimization of microgrids with renewable and storage energy systems. IEEE, International Conference on Environment and Electrical Engineering.
28. Yeh EC, Venkata SS, Sumic Z (1996) Improved distribution system planning using computational evolution. *IEEE T Power Syst* 11: 668–674.
29. Konfrst Z (2004) Parallel genetic algorithms: advances, computing trends, applications and perspectives. Parallel and Distributed Processing Symposium. Proceedings. International. IEEE, 162.
30. Buehren M. MATLAB Library for Parallel Processing on Multiple Cores. Available from <http://www.mathworks.com>.

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31. Kieny C, Berseneff B, Hadjsaid N, et al. (2009) On the concept and the interest of Virtual Power plant: Some results from the European project FENIX. Power & Energy Society General Meeting, IEEE, 1–6.



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